Investigation of Complex Formation in the Systems $MnCl_2$ - SOV/78-3-10-31/35-LiCl- H_2O , $CoCl_2$ - $KCl-H_2O$ and $AlCl_3$ - $KCl-H_2O$

of the density from the additivity is insignificant since the initial solutions have almost the same density. It was made absolutely clear by the refractometric method that molecular compounds exist in the ternary systems analyzed. There are 3 figures, 1 table, and 5 references, which are Soviet.

SUBMITTED:

July 17, 1957

Card2/2

YERMOLENKO, N.F. [IArmolenka, M.F.]; DEYCH, A.Ya. [Deich, A.IA]; LEVITMAN, Kh.Ya. [Levitman, Kh.IA]

Molecular compounds in ternary and binary mixtures based on refraction and density factors. Vestsi AN BSSR. Ser. fiz.-tekh. nav. no.1:25-29 '59. (MIRA 12:6) (Systems (Chemical))

CIA-RDP86-00513R000410310014-7 "APPROVED FOR RELEASE: 06/12/2000

sov/78-4-5-41/46 5(4) Deych, A. Ya., Nasonov, V. S. AUTHORS: Physico-chemical Analysis of the System CoCl2-CO(NH2)2-H20 TITLE: (Fiziko-khimicheskiy analiz sistemy CoCl2-CO(NH2)2-H2O) Zhurnal neorganicheskoy khimii, 1959, Vol 4, Nr 5, PERIODICAL: pp 1198-1201 (USSR) In the system $CoCl_2-CO(NH_2)_2-H_2O$ the optical density, surface ABSTRACT: tension, viscosity, and density were investigated. The initial solutions of CoCl and CO(NH2) were produced from chemically pure preparations with concentrations of 1.5 g-mol. Table 1 shows the results obtained by investigating optical density, surface tension, viscosity, and density. Figure 1 shows the optical density of the system CoCl2-CO(NH2)2-H2O, which was determined by means of a green filter. Figure 2 shows the density (1), the deviation of density from additivity (2), viscosity (3), the deviation of the logarithm of viscosity from additivity (4), and the surface tension (5) of the system $CoCl_2-CO(NH_2)_2-H_2O$. The microphotograph of the crystals, the initial solution, and the mixture with the

APPROVED FOR RELEASE: 06/12/2000 CIA-RDP86-00513R000410310014-7"

Card 1/2

 $\frac{\text{SOV}/78-4-5\cdots41/46}{\text{Physico-chemical Analysis of the System CoCl}_2-\text{CO(NH}_2)_2-\text{H}_2\text{O}}$

molar ratio of components 1:1 were investigated. From the deviation from the additivity of density and the logarithm of viscosity it follows that the compound $\operatorname{CoCl}_2.\operatorname{CO(NH}_2)_2$ forms in this system. The microphotograph of the crystals

confirms the existence of this compound. There are 3 figures, 1 table, and 7 Soviet references.

SUBMITTED: February 20, 1958

Card 2/2

DEYCH, A.Ya.

Formation of compounds of higher order in the system GaCr₂O₇ - K₂Cr₂O₇ - H₂O_• Zhur.neorg.khim. 5 no.2:503-505 (Calcium dichromate) (Potassium dichromate) F 160.

S/078/60/005/009/038/040/XX B017/B058

AUTHOR: Deych, A. Ya.

TITLE: Study of the Systems MnCl₂ - LiCl - CH₃OH and ZnCl₂ - LiCl - CH₃OH by Means of Physico-chemical Analysis Methods

PERIODICAL: Zhurnal neorganicheskoy khimii, 1960, Vol. 5, No. 9, pp. 2111 - 2114

TEXT: The systems MnCl₂ - LiCl - CH₃OH and ZnCl₂ - LiCl - CH₃OH were studied by means of physico-chemical analysis methods. The systems were investigated at 20°C with regard to their viscosity, density, surface tension and optical density. The results are mentioned in Tables 1 and 2 and graphically represented in Figs. 1 and 2. In the system MnCl₂ - LiCl - CH₃OH, a hardly noticeable interaction of the components was established, especially by determining the optical density. An easily dissociable molecular bond of the composition Li[ZnCl₃] was determined in the system

Card 1/2

ZnCl₂ - LiCl - CH₃OH. In methanol, ZnCl₂ has a sharper tendency to form complex anions than MnCl₂. The author mentions S. M. Dubrovskiy. There are 2 figures, 2 tables, and 14 references: 12 Soviet, 1 US, and 1 German.

SUBMITTED: June 30, 1959

Card 2/2

18.7400, 5.2200

78238 sov/80-33-3-39/47

AUTHOR:

Deych, A. Ya

TITLE:

Brief Communications. Physico-Chemical Investigation of the Possibility of Formation of Complexes in the

System $Zr(SO_4)_2 - CS(NH_2)_2 - H_2O$

PERIODICAL:

Zhurnal prikladnoy khimii, 1960, Vol 33, Nr 3,

pp 732-734 (USSR)

ABSTRACT:

In view of the contradictory opinions concerning the feasibility of electrodepositing zirconium in aqueous solutions of its sulfate, the authors investigated the system $\text{Zr}(\text{SO}_4)_2\text{-CS}(\text{NH}_2)_2-\text{H}_2\text{O}$ in order to ascertain whether $\text{Zr}(\text{SO}_4)_2$ reacts with thiourea similarly to NiSO₄ (this journal, 1959, Vol 32, p 1872), forming readily dissociable

complexes. According to the data obtained with regard to viscosity, density, and surface tension

Card 1/2

Brief Communications. Physico-Chemical Investigation of the Possibility of Formation of Complexes in the System $Zr(SO_4)_2 - CS(NH_2)_2 - H_2O$

78238 sov/80-33-3-39/47

of the aqueous solution of zirconium sulfate and thiourea, no molecular compounds were formed. Hence, the addition of thiourea to the electrolyte will not produce any desirable effect on the quality of the zirconium deposit. There is I table; I figure; and 7 Soviet references.

SUBMITTED:

September 19, 1959

Card 2/2

DLYCH, A.Ya.

More about the study of liquid systems by means of the deviation of viscosity logarithms from additivity. Zhur, fiz.khim. 34 no.6:1382-1383 Je '60. (MIRA 13:7) (Viscosity) (Systems (Chemistry))

YERMOLENKO, N.F.; DEYCH, A.Ya.

Studying the system CuSO₄ - NH₂ClH₂COOH - H₂O by physicochemical analysis. Dokl.AN BESR 5 no.5:215-217 My '61. (MIRA 14:5)

1. Institut obshchey i neorganicheskoy khimii AN BSSR. (Copper sullate) (Clycide)

S/078/61/006/002/011/017 B017/B054

AUTHOR:

Deych, A. Ya.

TITLE:

Physicochemical Study of the Reaction of Zr(SO,)2 With Some

Organic Acids in Aquecus Medium

PERIODICAL:

Zhurnal neorganicheskoy khimii, 1961, Vol. 6, No. 2,

pp. 438 - 442

TEXT: The author studied the interaction of $Zr(SO_4)_2$ with quinic, maleic, and sulfosalicylic acid by determining the density, the viscosity, and the surface tension at 20°C. Results are given in Table 1. Fig. 1 shows density, viscosity, surface tension, and apparent volume of the precipitates in the systems $Zr(SO_4)_2$ - quinic acid - H_2O , $Zr(SO_4)_2$ - maleic acid - H_2O , and $Zr(SO_4)_2$ - sulfosalicylic acid - H_2O . Fig. 2 shows the surface tension of the system $Zr(SO_4)_2$ - quinic acid - H_2O , and that of zirconium sulfate solutions. Table 2 gives the surface tension in the system $Zr(SO_4)_2$ - Card 1/5

热

Physicochemical Study of the Reaction of 2x(SO₄)₂ S/078/61/006/002/011/017 With Some Organic Acids in Aqueous Medium

quinic acid - $\rm H_2O$. By determining the viscosity and the surface tension it was found that a chemical interaction takes place between the components in the systems $\rm Zr(SO_4)_2$ - quinic acid - $\rm H_2O$ and $\rm Zr(SO_4)_2$ - sulfosalicylic acid - $\rm H_2O$. No chemical interaction between the components was observed in the system $\rm Zr(SO_4)_2$ - maleic acid - $\rm H_2O$. A. K. Kirakosyan and I. V. Tanangev are mentioned. There are 2 figures, 2 tables, and 6 Soviet references.

SUBMITTED: December 8, 1959

Card 2/5

"APPROVED FOR RELEASE: 06/12/2000 CIA-

CIA-RDP86-00513R000410310014-7

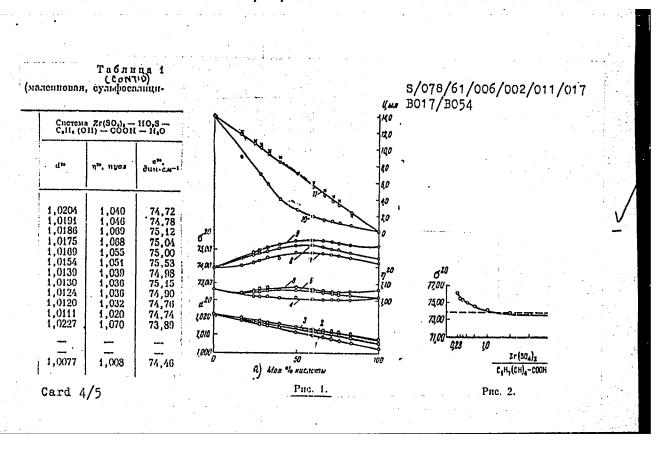
Card 3/5

S/078/61/006/002/011/017 B017/B054

11 потность, инжесть, ноперхностное натяжение и нажущиеся объемы оснанов в системах $Zr(SO_i)_2$ — хиппал донал) кислота — II_2O

THISTE !										
Кислота	Опплаемые панувриеся объемы осад- нов при от- суствии взаи- модействии помпонентия системы, ил	$\begin{array}{c} \text{CHCTEMA} \\ \text{Zr}(SO_4)_2 - C_4H_1(OH)_4 - COOH - H_2O \end{array}$				Система Ir(SO ₁) ₂ — НООС — CH = CH — COOH — И ₂ O				
No cascen Zr(SO ₄) ₄		d³•	η ²⁴ , π y 23	он. дин-с.н-1	Кансущий- сп объем осаднов, ма	ď.	n ^{ze} , nyas	guit-c'il-r	Казнуций- сп объем осаднов, мл	
1 1:5 2 1 1:3 3 1:2,5 4 1:2 5 1:1,5 6 1:1 7 1:5:1 8 2:1 10 2:5:1 2,5:1 10 3:1 11 ΣηSO ₄) ₂ —	11,65 10,49 10,02 9,32 8,27 6,99 5,59 4,66 3,96 3,50 2,33 14,00	1,0186 1,0178 1,0179 1,0167 1,0149 1,0147 1,0131 1,0111 1,0096 1,0086 1,0227	1,033 -1,042 1,050 1,075 1,043 0,075 1,048 1,052 1,048 1,048 1,048 1,070	74,60 74,75 75,00 75,10 75,20 75,55 75,53 75,61 75,53 75,61 75,32 75,27 73,89	9,0 7,8 6,4 5,7 3,9 2,5 1,6 1,6 1,6	1,0199 1,0176 1,0165 1,0165 1,0145 1,0145 1,0199 1,0099 1,0077 1,0065 1,0055 1,0227	1,052 1,032 1,030 1,026 1,026 1,012 1,010 1,003 1,021 1,021 1,029 1,070	74,22 74,30 74,35 74,70 74,52 74,82 74,69 74,70 74,72 74,72 74,52 73,89	11,00 10,6 10,3 9,9 9,1 7,0 6,0 5,2 4,1 4,0 2,4	
Хинная кислота Малениовая кислота Сульфосаницилован кис- лота	=	1,0058	1,056	75,24 — —	-	1,0017	1,019	74,17	1.	

"APPROVED FOR RELEASE: 06/12/2000 CIA-RDP86-00513R000410310014-7



S/078/61/006/002/011/017 B017/B054

Legend to Table 1: 1: No. of mixture, 2 cid, 3: expected apparent volume of the precipitate without interaction of components, 4: system, 5: poise, 6: dyn·cm⁻¹, 7: apparent volume of the precipitate, 8: quinic acid, 9: maleic acid, 10: sulfosalicylic acid
Legend to Fig. 1: a) mole% acid; I: $Zr(SO_4)_2 - C_6H_4(OH)_4COC' - H_2O$; II: $Zr(SO_4)_2 - C_2H_2(COOH)_2 - H_2O$; $Zr(SO_4)_2 - C_6H_3(OH)(HO_3S)COOH - H_2O$; density: 1 in system II, 2 in system I, 3 in system III; viscosity: 4 in system II, 5 in system III, 6 in system I; surface tension: 7 in system II, 8 in system III, 9 in system I; apparent volume of precipitate: 10 in system I, 11: expected volume of precipitate, X in system II

Card 5/5

DEYCH, A. Ya. (Riga)

Viscosity logarithm and reciprocal kinematic viscosity in the systems benzene - tolune and n-butyl alcohol - tert -butyl alcohol. Zhur. fiz. khim. 35 no.3:635-637 Mr *61. (MIRA 14:3) (Systems (Chemistry)) (Viscosity)

YERMOLENKO, N.F.; DEYCH, A.Ya.

Possibility of forming higher order compounds in the system AlCl3 - GS(NH₂)₂ - H₂O. Izv.vys.uch.zav.; khim.i khim.tekh. 5 no.4:536-538 '62. (MIRA 15:12)

1. Belorusskiy gosudarstvennyv universitet imeni Lenina, kafedra neorganicheskoy khimii, (Aluminum chloride) (Urea)

DEYCH, A.Ya.

Chemical reaction of urea with barium bromide in an awueous medium. Zhur.neorg.khim. 7 no.6:1421-1423 Je '62. (MIRA 15:6) (Urea) (Barium bromide)

DEYCH, A.Ya.

additive value of viscosity of liquid systems without interaction of components. Thur. fiz. khim. 36 no.3:656-657 Mr 162. (MIRA 17:3)

1. Highskiy institut inzhenerov Grazhdanskogo vozdushnego flota.

DEYCH, A.Ya.

Additivity of the viscosity logarithm and the reciprocal kinematic viscosity of binary liquid systems. Zhur.fiz.khim. 36 no.8:1777-1779 Ag '62. (MIRA 15:8)

1. Vsesoyuznyy zaochnyy institut tekstil'noy i legkoy promyshlennosti i Rizhskiy uchebno-konsul'tatsionnyy punkt.

(Systems (Chemistry)) (Viscosity)

DEYCH, A.Ya.

Density, viscosity, and specific conductivity of CdBr₂ solutions in acetone, water, and their mixtures. Zhur. fiz. khim. 36 no.ll:2479-2480 N.62. (MIRA 17:5)

DEYCH, A. Ya.; VORONKOV, M. G.;

"Donor-acceptor properties of the siloxane bond."

Institute for organic syntheses of the Latvian Academy of Science, Riga, USSR.

Second Dresden Conference on Organic and Non-Silicate Chemistry, 26-30 March 1963; East Germany.

VORONKOV, M. G.; DEYCH, A. Ya., Riga

"Acceptor complexes of monosubstituted benzenes C_6H_5X with electron donor organic compounds."

report submitted for 8th Intl Conf on Coordination Chemistry, Vienna, 7-11 Sep 64/

ACCESSION NR: AP4040730

s/0192/64/005/003/0482/0489

TITLE: Donor-acceptor properties of the silloxane bond

AUTHOR: Voronkov, M. G.; Deych, A. Ya.

SOURCE: Zhurnal strukturnoy khimii, v. 5, no. 3, 1964, 482-489

TOPIC TAGS: siloxane bond, alkoxysilane, aryloxysilane methylsiloxane, donor acceptor property, electro acceptor bond, electro donor bond, physico chemical method

Si-O bond in siloxanes and alkoxysilanes and to clarify the bond nature, more than 300 binary systems of alkoxysilanes, aryloxysilanes methylsiloxanes and their organic analogues with electro-acceptor and electro-donor bonds were analyzed by physico-chemical methods. It has been shown that both electro-donor and electro-acceptor properties of alkoxysilanes are enhanced by a decreasing number of alkoxygroups at the central silicon atom; this is explained by both the sterical factor and the increasing polarity of the Si-O bond. A new type of molecular interaction between alkoxysilanes and polar

APPROVED FOR RELEASE: 06/12/2000 CIA-RDP86-00513R000410310014-7"

ACCESSION NR: AP4040730

benzene derivatives of the C6H5X was found. The composition of stratified systems formed by methylsiloxanes with organic compounds was determined. Donor/acceptor properties of the siloxane bond Si-O-(Si) in siloxanes in relationship to organic molecules are usually not apparent and can but rarely be observed. Electrodonor properties decrease in the series $C-0-C>C_{alk}-0-Si>C_{ar}-0-Si>>Si-0-Si>(0)-Si-0-Si while the electro-acceptor properties of the silicon atom decrease in another order <math>Si_{ar}-0-Si>C_{alk}-0-Si>>Si-0-Si$. Detailed experimental data supporting the above conclusions will be published in a series of articles on this subject. Orig. art. has: 1 figure, 1 formula, 1 table.

ASSOCIATION: Institut organicheskogo sintema AN LatySSR (Institute of Organic Synthesis, AN LatvSSR) SUBMITTED: 17Mar63 ENCL: 00
SUB CODE: IC NR REF SOV: 005 OTHER: 004

2/2

DEYCH, A.Ya.

Some remarks concerning V.S. Galinker, V.A. Tiagai, G.N. Some remarks concerning v.s. Gullinker, v.H. lingal, c....
Fenerli's article "Viscosity of mixtures of aqueour electrolyte solutions." Zhur. fiz. khim. 38 no.2:525-527 F '6 W (MIR4 17:8)

1. Rizhskiy institut inzhenerev Grazhdanskogo vozdushnogo flota.

DEYCH, A.Ya.; VYAZOVSKAYA, A.B.

Some physicochemical properties of aminoacetic acid aqueous solutions. Zhur. fiz. khim. 38 no.4:980-983 Ap 164.

1. Rizhskiy institut inzhenerov Grazhdanskogo vozdushnogo flota.

L 12982-66 EWT(m)/EWP(1)/T RPL WW/RM

ACC NR. AP6001461 SOURCE CODE: UR/0379/65/001/005/0663/0674

AUTHOR: Voronkov, M. G.; Deych, A. Ya.

ORG: Institute of Organic Synthesis, AN Latv. SSR. Rips (Institut organicheskogo sinteza); Riga Institute of Civil Aviation Engineers (Rizhskiy Institut inzhenerov grazhdanskoy aviatsii)

TITLE: Formation of complexes with charge transfer in systems of monosubstituted benzenes C_6H_5X with electron-donor organic compounds

SOURCE: Teoreticheskaya i eksperimental'naya khimiya, v. 1, no. 5, 1965, 663-674

TOPIC TAGS: intermolecular complex, benzene, electron donor

ABSTRACT: The paper deals with the formation of labile complexes with charge transfer in systems of C_8H_8X monosubstituted benzenes with organic compounds (D) containing a hetero atom with an unshared pair of electrons (O, N, and Cl). Using refractometry, from the character of n(V) isotherms of over 400 liquid binary systems C_8H_8X -D, the authors found that the tendency of C_8H_8 molecules to form complexes is most pronounced if X is a meta-orientant, and increases with increasing dipole moment of the molecule. The complexing tendency of electron-donor components (D) decreases in the following order of variation of the hetero atom in D: C_8 - C_8 -

Cord 1/2

TO MOUNT OF	wis sume or	π electron	s. they m	r from ordin ay be terme	d Urouori	~~ ~ ~~~~ ~		mL .	-4	•
Tunanc su	nerion 1	s hosmrate	d. Orig.	during the in art. has: 3	figures a	nd 4 table	8.	nucleo	philic	
Ul3 CODE:	07 / SUBN	I DATE: 0	8Mar65 /	ORIG REF:	01.8 / O	TH REF:	015	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1		
							+ 11 1 - 1	•		
Ø-										
$\mathcal{O}(\mathcal{O})$							•			
d 2/2										

DEYCH, A.Ya.

Role of deviation from additivity in the study of complex formation in electrolyte solutions from viscosity data. Zhur. fiz. khim. 39 no.3:804-805 Mr 165. (MURA 18:7)

1. Rizhskiy institut inzhenerov grazhdanskoy aviatsii.

16.4000

37009 S/044/62/000/003/062/092 C111/C444

THOR: Deych, E. G.

TITLE:

On some infinite systems of equations

PERIODICAL:

Referativnyy zhurnal, Matematika, no. 3, 1962, 38,

abstract 3V191. ("Zh. vychisl. matem. i matem. fiz.", 1961,

<u>1</u>, no. 1, 173-176)

TEXT:

If the system

 $x_i = \sum_{k=1}^{\infty} c_{ik}x_k + b_i$ (i = 1,2,...) is completely regular (i.e.

 $\sum_{k=1}^{\infty} \left| \begin{array}{c} c_{ik} \\ \end{array} \right| < 1 - \theta < 1 \text{) and } \left| \begin{array}{c} b_i \\ \end{array} \right| < P, \text{ then this system possesses a}$

unique bounded solution, as it is well known, where $|x_1| \le k = P/Q$. It is proved that in case the coefficients c_{ik} and b_i being of the same sign, this estimation can be unproved:

1.) if $c_{ik} \leq 0$, $b_i \geqslant 0$, then $|x_i - b_i| \leq k \frac{1 - \theta}{2 - \theta}$ and $|x_i| \leq k \frac{1}{2 - \theta}$;

s/044/62/000/003/062/092 On some infinite systems of ... C111/C444
2.) if $c_{ik} \ge 0$, $b_i \ge 0$, then $b_i \le x_i \le b_i + k(1-\theta)$ and $0 \le x_i \le k$. The case $b_i \le 0$ is reduced to the considered case by aid of the substitution $x_k = -y_k$. [Abstracter's note: Complete translation.]

Card 2/2

8/040/62/026/005/010/016 1)234/D308

AUTHOR:

Deych, E. G. (Bucarest)

TITLE:

An axially symmetrical contact problem for a nonplane die with circular horizontal section

PERIODICAL: Prikladnaya matematika i mekhanika, v. 26, no. 5,1962, 931–934

TEXT: The author assumes that the elevation of the points of the die in the initial state over the upper plane of the elastic halfspace is given by

$$\varphi(\mathbf{r}) = A\mathbf{r}^{2\lambda} \qquad (\lambda > 0) \qquad (1.1)$$

and that a force Q is applied along the axis of the die. It is attempted to simplify the formulas for the radius of contact area (a), the displacement and the pressure distribution. The result is Card 1/2

An axially symmetrical

\$/040/62/026/005/010/016 D234/D308

$$a^{2\lambda+1} = \frac{(\nu-1)Q}{4\nu GA} \frac{T(\lambda+3/2)}{\lambda\sqrt{\pi}\Gamma(\lambda+1)}, \quad \delta = Aa^{2\lambda} \frac{\sqrt{\pi}\Gamma(\lambda+1)}{\Gamma(\lambda+1/2)} \quad (2.11)$$

$$p(r) = \left(\lambda + \frac{1}{2}\right) p^{o}\left(\frac{r}{a}\right)^{2\lambda-1} \sqrt{1 - \frac{r^{2}}{a^{2}}} F\left(\lambda + \frac{1}{2}, \frac{1}{2}; \frac{3}{2}; 1 - \frac{r^{2}}{a^{2}}\right)$$

$$(0 \langle r \langle a \rangle) \tag{3.9}$$

G being the displacement modulus of the half-space and $p^0 = Q/\pi a^2$. The first two expressions are derived from series expansions and the third from an integral representation. The particular cases $\lambda = 2n$, 1/2, 3/2 are analyzed. SUBMITTED: April 25, 1962 Card 2/2

USSR/Discuses of Farm Initals. Discuses Caused by Helminths

R

Abs Jour : Ref Zhur - Biol., No 19, 1958, No 88267

Author

: Deych F.F.

Inst

: Kuzakh Scientific Research Veterinary Institute

Title

: Experiment in Controlling Hemo-Onehocorcosis and Chabert's

Disease in Sheep of the Vostochne-Kazakhstanskaya Oblast.

Orig Pub : Tr. Kezelthsk. n.-1. vet. in-ta, 1957, 9, 464-463

Abstract : No abstract

Cord : 1/1

DEYCH, G. M.

Dissertation defended for the degree of Doctor of Historical Sciences in the Institute of History

"Peasantry of the Pskovskaya Giberniya During the Second Half of the XIX and at the Start of the XX Century."

Vestnik Akad. Nauk, No. 4, 1963, pp 119-145

SOV/113-59-3-18/22

28(1)

AUTHOR:

Petukhov, P.Z.. Professor, Doctor of Technical

Sciences Fedoseyev, A.M., Engineer and Deych, G. Sh.

TITLE:

On the Application of Forging Manipulators (O primenenii

kovochnykh manipulyatorov)

PERIODICAL:

Mekhanizatsiya i avtomatizatsiya proizvodstva, 1959,

Nr 3, pp 54-55 (USSR)

ABSTRACT:

An important part in machine building is played by forging work, and, therefore, the forging press departments of large plants are already and in future will be still more fully equipped with first-rate forging presses. Alloys, weighing tens of and even hundreds of tons, are forged by such presses. The transportation of heated alloys to the presses is carried out by bridge cranes. Experience shows, that presses with forging manipulators possess a rate of production 50-80% higher than that of presses with forging cranes. Their fuel consumption is lower by 10-20%. The authors are of the opinion, that presses with pressures of up to 3 tons, can be adequately

Card 1/2

SOV/1 18-59-3-18/22

On the Application of Forging Manipulators

operated by transporting cranes only. Having given a detailed account of production costs and the price of the machine itself, the authors conclude as follows: The State Technical Scientific Committee of the USSR of the Council of Ministers and the Gosplan should be given the task of finding the very best possibilities for complex mechanization of forging press departments, and specially for the construction of forging manipulators with various load capacities.

Card 2/2

BUKANKOV, Ye.I., inzh.; DEYCH, M.M.

Use of plastic heels without plugs. Kozh.-obuv.prcm. 6 no.10:34-35

O *64. (MIRA 18:1)

DEYCH, M. Ye.

"Question of Finite Losses in the Guide Channels of Steam Turbines." Sov. Kotlostroy. No. 6(1945)

DEYCH, M.Ye.

AID 400 - I TREASURE ISLAND BIBLICGRAPHICAL REPORT PHASE I

Call No.: AF623562 BOOK

Author: DEYCH, M. YE. TECHNICAL GAS DYNAMICS (FUNDAMENTALS OF TURBINE GAS Full Title:

DYNAMICS) Tekhnicheskaya gazodinamika (Osnovy gazo-Transliterated Title: dinamiki turbin)

Publishing Data

Originating Agency: None

Publishing House: State Power Engineering Publishing House Date: 1953 No. pp.: 544 No. of copies: 5 No. of copies: 5,000

Editorial Staff

Tech. Ed.: None Editor: None Appraiser: None

Editor-in-Chief: None Others: The author thanks a number of scientists and engineers

for help and mentions their names in the introduction.

Text Data

Coverage: In this book some fundamental problems of internal gas dynamics of the turbine are considered. The initial chapters cover the elements of the theory of one-dimensional and two-dimensional The following chapters are dedicated to special problems of internal gas dynamics, namely the flow of gas in nozzles, labyrinths, ejectors, bladings and the turbine stage. Special attention is given 1/7

Tekhnicheskaya gazodinamika (Osnovy gazodinamiki turbin)

AID 400 - I

to the gas dynamics of alternating cycles of nozzles, ejectors, and turbine stage. In the concluding chapters methods are given for experimental testing of the turbine section between the inlet and the outlet. Diagrams and graphs.

This is a good textbook on fluid dynamics as applied to gas turbines. It contains a large amount of material. However, the approach to the problems studied is conventional and no special features or original solutions have been noticed.

TABLE OF CONTENTS
Preface

PAGES

Introduction

3-7 8-14

Ch. I Basic Equations of Gas Dynamics. Linear Flow of a Gas at Constant Entropy

5-46

1-1. Flow parameters; 1-2. Equation of continuity; 1-3. Equation of the quantity of movement in the projection on orthogonal axes of a system coordinates; 1-4. Equation of energy; 1-5. Euler's equations for linear flow; 1-6. Speed of sound; 1-7. Multiple forms of the equation of energy; 1-8. Flow parameters in an arbitrary section of the stream tube; 1-9. Change of velocity along the stream tube. Reduced discharge of gas.

2/7

Tekhnicheskaya gazodinamika (Osnovy gazodinamiki turbin)

AID 400 - I PAGES

Ch. II Two-dinemsional Movement of the Gas at Constant Entropy

47-100

2-1. Some basic conceptions of fluid dynamics. Vortex movement and circulation movement of a liquid. Velocity circulation; 2-2. Irrotational movement of a liquid; 2-3. Presure coefficients. Critical number M; 2-4. Taking account of the influence of compressibility by the method of small disturbances; 2-5. Correction for the influence of compressibility on a two-dimensional flow according to Khristianovich, S. A.; 2-6. Zhukovskiy's theorem; 2-7. Two-dimensional supersonic flow; 2-8. Diagram of characteristics; 2-9. Intersection and reflection of rarefication waves.

Ch. III Shock Waves in a Gas Flow
3-1. Shock wave formation; 3-2. Equation of oblique shock
waves; 3-3. Shock polaris; 3-4. Change of entropy in shocks;
3-5. Losses in shock waves. Wave resistance. Shock polaris
in a thermal diagram "is"; 3-6. Intersection of shock
waves; 3-7. Stepped drag of a flow; 3-8. Shock repercussion;
a) repercussion from a solid wall, b) repercussion from a
free boundary of streamlines; 3-9. Interaction of the shock
and the rarefication wave; 3-10. Conical shock waves.

3/7

Tekhnicheskaya gazodinamika (Osnovy gazodinamiki turbin)

AID 400 - I PAGES

Ch. IV Motion of Gas with Friction
4-1. Linear flow of gas with friction. Basic equations;
4-2. Motion of gas in a cylindrical pipe; 4-3. Losses due
to friction in a cylindrical pipe. Experimental data;
4-4. Boundary layer. Easic conceptions; 4-5. Integral correlation for the boundary layer; 4-6. Calculation of the
laminar boundary layer on a flat partition; 4-7. Conditional
depth of boundary layer. Second form of the integral correlation for the boundary layer; 4-8. Calculation of the
turbulent boundary layer; 4-9. Boundary layer at higher
velocities; 4-10. Resistance of bodies at subsonic and
supersonic velocities.

Ch. V Outflow of Gas from Convergent Nozzles and Openings.

Labyrinth Contractions

5-1. Convergent nozzle; 5-2 Convergent nozzle at variable operating conditions; 5-3. Flow of gas in a system of consecutive connection of convergent nozzles; 5-4. Discharge of gas at consecutively connected convergent nozzles; 5-5. Outflow of gas through an opening with a sharp rim. Second critical relationship of pressure; 5-6. Labyrinth convergence.

4/7

Yellinicheskaya gazodinamika (Osnovy gazodinamiki turbin)

AID 400 - I PAGES

Ch. VI Laval Nozzle and Diffusors. Stage of an Ejector 6-1. Calculation of supersonic nozzle; 6-2. Flat Laval nozzle at uncalculated conditions; 6-3. Conical Laval nozzles; 6-4. Supersonic nozzle with an oblique cut; 6-5. Diffusors: a) subsonic diffusor, b) supersonic diffusor; 6-6. Stage of the ejector; 6-7. Stage of the ejector at changeable operating conditions; 6-8. Choice of the geometrical parameters of the stage of the ejector. Ch. VII The Flow of Gas through Bladings of Turbo-Engines 312-419 7-1. Geometrical and gas dynamical blading parameters; 7-2. Theoretical methods of study of a two-dimensional potential flow of an incompressible fluid through bladings; 7-3. Electrical and hydrodynamic analogy; 7-4. Forces

7-2. Theoretical methods of study of a two-dimensional potential flow of an incompressible fluid through bladings; 7-3. Electrical and hydrodynamic analogy; 7-4. Forces acting on the profile in the blading. Zhukovskiy's theorem for the blading; 7-5. Basic characteristics of bladings; 7-6. Losses due to friction in two-dimensional blading at subsonic velocities; 7-7. Rim losses in two-dimensional bladings at subsonic velocities; 7-8. Some results of experimental study of two-dimensional bladings at low subsonic velocities; 7-9. Flow of gas through bladings at high subsonic velocities. Critical number M for a blading;

5 /7

Tekhnicheskaya gazodinamika (Osnovy gazodinamiki turbin)

AID 400 - I PAGES

7-10. Profile losses in bladings at higher subsonic velocities; 7-11. Flow of gas through reaction bladings at above critical jumps of pressure; 7-12. Operating bladings in supersonic flow; 7-13. Losses in bladings at transsonic and supersonic velocities; 7-14. Calculation of the deviation angle of flow in an oblique cut of the reaction blading at above critical jumps of pressure; 7-15. Special features of a three-dimensional flow in bladings.

Ch. VIII Some Properties of the Flow of Gas in the Stage of the Turbine

420-491

8-1. Basic equations; 8-2. Parameters of the flow in an absolute and relative motion; 8-3. Stage processes in the thermal diagram and the characteristics of stages; 8-4. Reduced discharge of gas through the moving blading; 8-5. Stage of the axial turbine with long blades;

8-6. Stage of the turbine at changeable conditions of operation. Parameters and equations of changeable conditions of operation; 8-7. Graphic of the changeable condition of operation of the stage of the turbine.

Ch. IX Methods of Experimental Study of the Turbine Section between Inlet and Outlet

492-536

6/7

Tekhnicheskaya gazodinamika (Osnovy gazodinamiki turbin)

AID 400 - I PAGES

9-1. Short characteristic of study methods and principal layouts of testing stands; 9-2. Installations for testing bladings under static conditions; 9-3. Fittings for measuring flow parameters; 9-4. Visual methods of flow study in bladings; 9-5. Some problems of method of study of flat bladings; 9-6. Experimental turbine.

Appendix, Table of Gas Dynamic Functions Bibliography

537-541 542-544

Purpose: This is a textbook in heat engineering approved by the Main Administration of Higher Education of the Ministry of Culture of the USSR. It may be used by students of senior courses, and also by technical workers of turbine construction plants and design bureaus.

Facilities: Some names of research institutes are mentioned.
No. of Russian and Slavic References: A number of articles and books are listed for each chapter of the book.
Available: A.I.D., Library of Congress.

7/7

DEYCH, M. Ye.

"The Flow of Gas Through Turbine Bucket Grids" Gosudarstvennoye Energeticheskoye Izdatel'stvo, Moscow-Leningrad, 1953, pp 312-420, 542-544.

Translation of Chapter VII of Tekhnicheskaya Gazodinamika, 568478

DEYCH, M. Ve.
SAMOYLOVICH, Georgiy Semenovich; TROYANOVSKIY, Boris Mikhaylovich; MICH,
M.Yo., redaktor; SHCHMCLYAYEV, A.V., redaktor; PRIDKIH, A.M., VOKAnicheskiy redaktor.

[Variable working cycle of steam turbines] Peremennyi reshim maboty parovykh turbin. Pod red. A.V.Shcheglineva. Moskva, Gos.energ.isd-vol 1955, 280 p. [Microfilm] (MIRA 8:5)

1. Chlen-korrespondent AN SSSR (for Shcheglyayev). (Steam turbines)

DEYCH, M. YA.

AID P - 2870

Subject

: USSR/Engineering

Card 1/1

Pub. 26 - 3/16.

Authors

: Deych, M.Ye., Kand. Tech. Sci., and Zaryankin, A.Ye.,

T1tle

: Research and improvement of nozzle plates of the control

stage

Periodical: Teploenergetika, 10, 14-20, 0 1955

Abstract

: Some results of research on mozzle plates, made in order to compare the operation of the two main types (the narrowing and the widening profile) are discussed. The research method, the characteristic of the nozzle plates, and the results achieved are explained in

detail. Twelve diagrams. One Russian reference, 1954,

1 German, 1910.

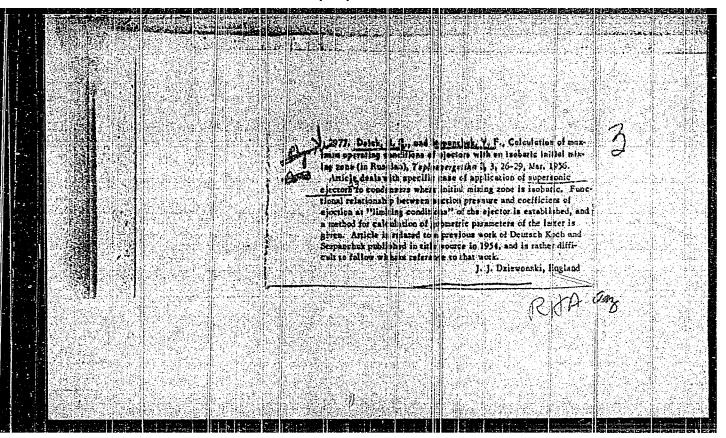
Institution: Moscow Power Institute

Submitted : No date

DEYCH, N.Ye.

[Experimental studies and the principles of aerodynamic calculation of steam and gas turbine stages] Eksperimental nye issledovania i osnovy aerodinamicheskogo rascheta stupenei parovykh i gazovykh turbin. Avtoreferat disserte sii na solukanie uchenoi stepeni doktora tekhnicheskikh nauk. Moskva, Moskovskii ordena Lenina energeticheskii institut im. V.M.Molotova, 1956. 42 p. (MIRA 10:3) (Purbines--Aerodynamics)

"APPROVED FOR RELEASE: 06/12/2000 CIA-RDP86-00513R000410310014-7



DETEN, ME.

AID P - 4224

Subject

: USSR/Heat and Power Engineering

Card 1/1

Pub. 110 a - 5/15

Authors

: Deych, M. E. and V. F. Stepanchuk, Kands. Tech. Sci.

Title

: Computing operational limits of ejectors with an

initial isobaric mixture (stage).

Periodical: Teploenergetika, 3, 26-29, Mr 1956

Abstract

: The article reports on experimental data obtained on supersonic ejectors and gives a detailed analysis for the computation of formulae for indraft pressure for the limit of the ejection ratio and of the limit of

back pressure. Four diagrams.

Institution: Moscow Power Engineering Institute

Submitted : No date

Degch, M. E

AID P - 4377

Subject

: USSR/Power Engineering

Card 1/1

Pub. 110 a - 3/17

Authors

: Deych, M. E., V. V. Frolov, Kand. Tech. Sci., and A. V. Gubarev, Eng., Moscow Power Enstitute

Title

: Research on new shapes of cascades and pressure stages

in turbines.

Periodical: Teploenergetika, 5, 13-22, My 1956

Abstract

: Experiments with a series of bladings of new shapes including research at supersonic velocity, are described. Basic aerodynamic data of new blading are given. Mathematical analyzes of various control and pressure stages designs are presented. Twelve figures, 6 tables..

Institution: None

Submitted : No date

Name: DEYCH, Mikhail Yefimovich

Dissertation: Experimental studies and bases of aerodynamic

calculation of stages of steam and gas turbines

Degree: Doc Tech Sci

Affiliation: __not indicated_]

Defense Date, Place: 26 Oct 56, Council of Moscow Order of Lenin Fower

Engineering Inst

Certification Date: 18 May 57

Source: BMV0 15/57

43

DEYCH, M. YE.

BARANOV, V.A., kandidat tekhnicheskikh nauk; DilYCH, M.Te., kandidat tekhnicheskikh nauk.

Experimental apparatus for determination of grate characteristics by the method of reactive power weighting. Teploenergetika 4 no.3: 28-31 Mr 157. (MLRA 10:3)

1. Moskovskiy energeticheskiy institut.
(Boilers-Testing)

Deych, M.F.

AUTHORS:

Shcheglayev, A. V. (Corresponding Member Ac.Sc. USSR) and Deych, M.E. (Cand. Tech. Sc.) (Moscow Power Institute)

TITLE:

Certain questions relating to increasing the efficiency of steam turbines. (Nekotorye voprosy povysheniya ekonomichnosti parovykh turbin).

PERIODICAL: "Teploenergetika" (Thermal Power), Vol.4, No.4, April, 1957, pp. 3 - 6 (U.S.S.R.)

ABSTRACT:

Most of the work that has been done on aerodynamics of the flow parts has been concentrated on the intermediate stages. It is quite recently and only in the Moscow Power Institute that the regulating stages have been investigated, whilst the treatment of low pressure stages with small d/l ratios at high subsonic and supersonic speeds has hardly been commenced. In this article the authors consider some questions of the efficiency of steam turbines and of the losses which are associated with design and manufacture in order to judge of the best directions for future research. With the use of high steam conditions leakages acquire particular importance. Leakages may occur in the fixings of the nozzle segments of the regulating stages. Leakage can occur through butt joints and it is particularly difficult to make a steamtight joint around the edges Leakages can also occur around diaphragms of segments. and particularly at the annular surface where the

Certain questions relating to increasing the efficiency of steam turbines. (Cont.)

diaphragm joins the frame. It is particularly important to maintain in operation minimum clearances at the glands. In many turbines the glands wear, and this increases losses from steam leakage. Correct selection of the regulating stages has a considerable influence on the efficiency of a turbine. In turbines with high initial steam temperature the regulating stage should be designed for a considerable heat drop. Curtis wheels with two rows of blading which have been used in these stages in the past do not have high enough efficiency and new turbines are being designed with a single row of blades on this wheel. However, work has recently been done in the Moscow Power Institute to improve the efficiency of wheels with two rows of blading and efficiencies of 72 to 75% have been obtained. Therefore. it may be again advisable to use such stages in some types of turbine for high steam conditions. The work which has been done on the intermediate stages of turbines has resulted in satisfactory efficiency. However, available data suggests that it is not always possible to find the best solution which gives the smallest loss due to flow of steam over the binding on the working blades, and improvements in this respect could be achieved.

Certain questions relating to increasing the efficiency of steam turbines. (Cont.)

Little work has been done on the low pressure section. Such theoretical investigations as there have been have included simplifying assumptions. Practically all the methods of profiling long blades do not allow for important special features of the actual spatial flow in such stages. Experimental investigation of stages with low d/l ratio are mainly carried out on air models of turbines. These results cannot easily be extended to a group of low pressure stages because the tests are carried out at relatively low speeds whilst in real stages the velocities are either subsonic or Tests in power stations have shown that the efficiency of the later stages of high power turbines is low. More attention is required to the design of blading for low pressures and very high speeds. The use of Baumann two row stages for high power turbines requires further consideration. Operating tests have shown that the live steam governing valves operate with high losses. Investigations should be directed to developing valves of better aerodynamic shape and diffusors that will reduce losses to a minimum. Difficulties arise because laboratory investigations are often carried out on model installations which cannot fulfil all the requirements of similarity.

Certain questions relating to increasing the efficiency of steam turbines. (Cont.)

necessary to develop practical questions of modelling so that the main requirements of similarity are fulfilled. Finally, it is most important to make full scale tests on new and reconstructed turbines in power stations. Insufficient attention is being paid to this matter. It is surprising that the Kharkov turbine works still has no laboratory and that the Leningrad works has not used for experiments a high pressure Heat and Electric Power Station that is on its very doorstep. No figures, no literature references.

Deych, M.E. (Cand. Tech. Sci.), Samoylovich, G.S. (Cand. Tech.Sci.), Troyanovskiy, B.M. (Cand. Tech. Sci.), Kazintsev, F.V. (Engineer) and Lipatnikov, S.N. (Eng.) .AUTHORS:

Investigation of two-crown regulating stages in an TITLE:

experimental steam turbine. (Issledovaniye dvukhvenechnykh reguliruyushchikh stupeney v parovoy eksperimental'noy

turbine).

PERIODICAL: "Teploenergetika" (Thermal Power), Vol.4, No.5, May, 1957,

pp.35-43 (U.S.S.R.)

Operating test results have shown that the regulating ABSTRACT: stages having two sets of blading on a single runner that are used by steam turbine factories are of low

efficiency. Therefore, turbine designers try to avoid the use of such stages in high power turbines.

hitherto, such stages have not been systematically

investigated, the reasons for their low efficiency have

not been established and methods of improving the efficiency have not been indicated. This article describes new 2-crown regulating stages that have been developed in the Moscow Power Institute intended for various heat drops and steam consumptions. The explanations of the type of stage and of the experimental conditions are all expressed

in terms of Soviet conventional notation which is assumed to be so familiar to the reader as to require no explanation.

The experimental set-up is described, the available experimental turbine having the following limiting

629

Investigation of the two-crown regulating stages in an experimental steam turbine. (Cont.)

conditions: maximum power 600 kW, maximum speed 12 000 r.p.m.; initial pressure 1 to 5 atm.; maximum initial temperature 150 to 300°C and exhaust pressure 0.1 to 2 atm. The turbine is loaded by a hydraulic brake. The main geometrical characteristic of the stages tested are described with full information about blade profiles and dimensions. The results of the tests are presented in the form of graphs of the internal and blade efficiencies.

The experiments carried out were of a preliminary nature. For a number of operational reasons unstable conditions were obtained with a deep vacuum beyond the stage and it was, therefore, impossible to obtain a reliable efficiency value for certain conditions and particularly for low Reynolds numbers. Moreover, the relative error of the experiment is higher with deep vacuums because the power of the stage is less. However, the test results are of interest in that they give a qualitative picture of the relationship between efficiency and Reynolds number. Graphs illustrating this point are given. Information is also given about changes in the reaction under different conditions and the results of investigations on the stages with partial supply of steam. Some results are also given on a

Investigation of the two-crown regulating stages in an experimental steam turbine. (Cont.)

detailed investigation of the structure of flow in the stages, including graphs of pressure distribution over the profile of the blading.

It is concluded that stage type KS-lA is of high efficiency over a fairly wide range of conditions. With partial supply of steam the blade and internal efficiencies of the stage are reduced. Protective housings and longitudinal glands on the boundaries of the arc of steam supply should be installed to reduce windage losses. General agreement was found between the pressure distributions over the profile determined under static conditions and by calculations. There is reason to think that similarity of pressure fields is observed during tests using steam and air. 11 figures, 1 literature reference (Russian).

Card 3/3

96-58--2-20/23

AUTHOR: Deych, M.Ye., Doctor of Technical Sciences

. . . .

TITLE: A Coordinating Conference on Investigations on the Flow Part of Steam Turbines (Koordinatsionnoye soveshchaniye po issledovaniyam protochnoy chasti parovykh turbin)

PERIODICAL: Teploenergetika, 1958, No 2, pp 91 - 93 (USSR)

This is a brief account of a conference called by the ABSTRACT: Steam Turbine Section of the High Pressure Steam Commission of AS USSR (Kommissiya para vysokogo davleniya AN SSSR) and neta in Moscow from October 8 - 11, 1957. The conference was attended by representatives of the leading factories and research and teaching institutes. The results of investigations on the flow parts of steam turbines carried out during 1956-57 and the plan of work for 1958-1962 were considered. The conference noted that a particularly important development of recent times had been the extension of existing works laboratores and the organisation of a number of new ones. Reports were made of investigations on regulating stages. Particular reference was made to the work done to raise the efficiency of double-row regulating stages. The efficiency of 100 and 150 MW turbines has been appreciably increased by re-design of the regulating stages.

Gardl/3 Numerous reports dealt with increasing the efficiency of

A Coordinating Conference on Investigations on the Flow Part of **96-58-**2-20/23 Steam Turbines

intermediate stages. A report was made on the preparation of standard blade profiles for intermediate stages and another on the testing of intermediate stages in experimental turbines. There was also an account of work on stages with long, twisted blades.

A good deal has been done to modernise existing sets, applying recent research work. The manufacturing shops have made numerous tests on prototypes.

The conference approved the main directions of work on regulating and intermediate stages but pointed out that there had been insufficient theoretical and experimental attention to the following subjects: modelling of blading, exhaust sections and valves; study and improvement of the later stages of turbines and experimental work on the degree of reaction and other design features of intermediate stages. The conference emphasised the importance of evolving a more accurate procedure for the thermal design of the flow part of steam turbines. This work is going slowly. Investigations on turbines installed in power stations are being made by only three organisations and not enough is being done. Co-ordination of work between different laboratories is

Card2/3 weak and the conference took special decisions on this question.

96-58-2-20/23

A Co-ordinating Conference on Investigations on the Flow Part of Steam Turbines

In conclusion, the conference considered and confirmed the proposed thematic plan of research work to raise the efficiency of steam turbines for the period 1958-1962.

AVAILABLE:

Library of Congress

Card 3/3

1. Steam turbines-Characteristics

GUBAREV, A.V.; DEYCH, M.Ya.

Ceftain features of a supersonic flow in active cascades. Nauch. dokl. vys. shkoly; energ. no.2:163-170 *58. (MIRA 11:11) (Cascades (Fluid dynamics))

DEYCH, M.E.

TITLE:

96-3-6/26

AUTHOR: Deych, M.E. (Dr. Tech.Sci.) & Zaryankin, A.E. (Cand. Tech.Sci.)

An experimental investigations of the turbulent boundary layer at high subsonic speeds. (Eksperimental'noye issledovaniye turbulentogo

pogranichnogo sloya pri bol'shikh dozvukovykh skorostyakh.)

PERIODICAL: Peploenergetika, 1958, No.3. pp. 21-25 (USSR)

ABSTRACT: In order to investigate the turbulent boundary layer at high subsonic speeds the Moscow Power Institute set up the rig illustrated

diagrammatically in Fig.1. The boundary layer investigated was set up on the straightground section of the upper insert 1. To ensure that the boundary layer was turbulent a shallow groove was cut. A micro-nozzle was fitted 120 mm from the groove. The micro-nozzle was positioned by means of a micrometer screw. The installation could be used to determine the characteristics of the boundary layer during independent change in the M and Re numbers and the pressure gradient. The magnitudes determined by direct measurement were the initial pressure, the pressure of complete retardation in the boundary layer, the temperature of complete retardation, the static pressure along the investigated surface and the static pressure across the boundary layer at the section where the nose of the micro-probe was. In almost all of the tests the change of the static

probe was. In almost all of the tests the change of the static pressure in the boundary layer was small. Several equations required in the work are formulated. Fig.2. gives six velocity

Card 1/4 profiles obtained at a constant Reynolds number of 2.5 x 106 with the

90-3-6/26

An experimental investigation of the turbulent boundary layer at high subsonic speeds.

number M variable. All the experimental points within the range M=0.31-0.98 lie on a single curve, an expression for which is given; without great error the curve can be replaced by a straight line, the formula for which is given. Other formulae are, of course, possible, and any relationship that satisfactorily approximates the velocity profile in the boundary layer of an incompressible liquid can be extended to a flow of compressible fluid. The extrapolation need not be limited to sonic speed but can be extended to low supersonic speeds, but in this case it is difficult to obtain pure gradientless flow. From the results it is also possible to calculate values of the integral thicknesses of the layer and to construct curves of them as a function of M as shown in Fig. 3. The scatter of experimental points near sonic speeds occurs because of 'confusor' type flow. The scatter of points at subscnic speeds occurs because the points relate to different values of Reynolds number. The experimental results are in full accordance with theory. Experimental values for the height of the boundary layer for different values of M are given in Fig.4. On nearing the senic speed the reduction in thickness of loss of impulse is about 15%. Since the velocity profile is independent of M it may be supposed that Re is the main parameter that determines the velocity profile

Card 2/4

95-3-5/25

An experimental investigation of the turbulent boundary layer at high subsenic speeds.

in the absence of a pressure gradient, and the results of numerous experiments on its influence in an incompressible fluid can be extrapolated to a flow in a compressible flyid. Fig. 5. gives six velocity profiles obtained whilst varying Re whilst keeping M constant. Increase in Re from $0.61-1.08 \pm 10^6$ causes a characteristic change in the velocity profile, but further increase in he does not cause a change in the velocity profile. Therefore, for values of Re greater than about 1 x 100 the velocity profiles are expressed by the general relationship Eq(6). At high speeds the influence of Re on the turbulent boundary layer is qualitatively of the same order as in flows of incompressible fluid. To investigate the influence of M in the presence of a pressure gradient, velocity profiles were determined in the diffusor region (Fig.6A) and during 'confusor' flow Fig. 6B. The curves show that all the experimental points fall on a single curve, whatever the value of M. This confirms the conclusion that at subsonic speeds change in M does not cause appreciable change in the velocity profile. The influence of compressibility on the structure of the turbulent boundary layer is indirect. Change in the longitudinal pressure gradient, from a positive to a negative value, leads to considerable deformation of the velocity profiles and is clearly seen from the curves in Fig. 7. From the curve given in Fig. 8. it follows that when the velocity distribution at the outer edge of the boundary layer is

Card 3/4

An experimental investigation of the turbulent boundary layer at high subsonic speeds. 96-3-6/26

approximately linear calculations by the single parameter method are justified. A more general conclusion cannot be drawn in the absence of experimental data relating to other values of the second differential coefficient. There are 8 figures and 3 literature references (Russian).

ASSOCIATION: Moscow Power Institute (Moskovskiy Energeticheskiy Institut).

AVAILABLE: Library of Congress.

Card 4/4

DEYCH. M.YO.; BARANOV. .V.A.; ROZANOV. .K.A.

Investigating cascades of profiles of turbines by weighing the reactive power. Nauch.dokl.vys.shkoly; energ. no.3:139-148

[58. (MIRA 12:1)

DEYCH, M.Ye.; ZAMYANKIN, A.Ye.; SHERSTYUK, A.N.; DINEYEV, Yu.N.

Investigation of gate mechanisms of radial-flow turbines. Nauch.dokl.vys.shkoly; energ. no.4:195-206 158.

(MIRA 12:5)

1. Rekomendovana kafedroy parovykh i gazovykh turbin Moskovskogo energeticheskogo instituta.
(Gas turbines)

Deych, M.Ye., Doctor of Technical Sciences, Troyanovskiy, B.M., Candidate of Technical Sciences and Kazintsev, F.V., Abramov, V.I., Engineers AUTHORS: SOV/96-58-5-2/27

TITLE: Comparative Tests on a Two-row Velocity Stage (Sravnitel'nyye issledovaniya dvukhvenechnykh stupeney skorosti) PERIODICAL:

Deploenergetika, 1958, Nr 5, pp 9 - 16 (USSR). ABSTRACT:

Work done at the MEI (Moscow Power Institute) has led to the development of several two-row velocity wheels. One of these, stage KS-1A, was thoroughly tested in the experimental steam turbine of the Moscow Power Institute. The experimental procedure and test mesult were described in an article in Teploenergetika, 1957, Nr 5. They relate to a wheel with a mean diameter of 400 mm and a nozzle height of 15 mm and another with a diameter of 534 mm and height of 20 mm. Tests were also made on a stage, type KS-1A-3, with a wheel diameter of 668 mm and nozzle height of 25 mm. Curves of the internal efficiency of this stage with full steam supply are given in Figure 1. Thus, test results were obtained on three identical stages with constant d/2 ratio and different absolute values of d and ? As will be seen from the table, the area ratios differed for each stage and this affected the stage reaction to some extent. Graphs of the mean total reaction for velocity stage

Comparative Tests on a Two-row Velocity Stage SOV/96-58-5-2/27

KS-lA are given in Figure 2. The results of the tests on the three stages are then compared. The effect of blade height on stage efficiency is shown in Figure 3. It is of particular interest to compare the results for the new stages with best Soviet and foreign practice. Therefore, a detailed investigation was made of a two-row stage, type Nr 113, manufactured by the IKZ. The dimensions and clearances of stages KS-1A-3 and stage Nr 113 are given in dimensioned sketches, rigure 4. Test results for stage Nr 113 with full steam supply are given in Figure 5. The maximum internal efficiency was 71%: the total mean reaction of the stage, plotted in Figure 6,7In practically linear relationship with the velocity ratio and increases with increase of the heat drop on the stage. The steam consumption of stage Nr 113 is plotted in Figure 7. Tests were also made with different axial gaps. When the axial gap between the outlet edge of the nozzle and the inlet edges of the working blades of the first row is altered from 2.5 to 5.5 mm, the stage efficiency falls, as shown in Figure 8. The tests were made with the radial and all other Card2/5 ears constant.

Comparative Tests on a Two-row Velocity Stage

SOV/96-58-5-2/27

Investigations were then made on stage Nr 113 with steam supplied over only part of the arc; the gaps were unchanged and no special shields were used. The effect of partial steam-supply on the internal efficiency is showh graphically in Figure 9 and data on the mean total stage reaction are given in Figure 10. It follows from the results that different procedures should be used in selecting the design stage reaction for full and for partial steam supply. Velocity stages with expanding nozzles are used for operation at high supersonic drops. Two-row stages with expanding nozzles were investigated. One had the same working and guide blades as type or 113 with contracting nozzles as described above; the other had straighter-bladed guide vanes similar in shape to those of a compressor. The blade geometry is The graph of internal efficiency for stage Nr 113 with expanding nozzles and full steam supply is given in Fig 11. The efficiency is appreciably lower than for a stage with The efficieny and test results of different velocity/are then compared, noting, however that the procedures are still Card 3/5

Comparative Tests on a Two-row velocity Stage

SOV/96-58-5-2/27

insufficiently developed. Even stages tested in one and the same turbine differ in their geometrical characteristic in a way which affects the efficiency. various methods are used in this article to compare velocity stages, Internal efficiency curves with full steam supply for all stages are shown in Figure 12: all stages were tested in the same experimental turbine, using the same procedure. The best mesults were obtained with the Moscow Power Institute stage KS-1A-3 with a mean wheel diameter of 668 mm and a nozzle height of 25 mm. Here, the maximum efficiency is 81% but cannot be compared directly with stage Nr 113 because of the considerable difference in dimensions. However, if the curves of the KGTZ (Khar'kov Turbo-generator Works) are used to recalculate the results for stage Nr 113 to the dimensions of stage KS-1A-3, its efficiency is increased by only 2.5% and becomes 73.8%. The stage efficiencies of different wheels are then discussed; the internal efficiencies of velocity stages KS-1A-2 (with welded diaphragm) and of stage Nr 113 as a function of nozzle area are given in Figure 13. Throughout the range, the efficiency of stage KS-1A-2 is Card 4/5

sov/96-58-5-2/27

Comparative Tests on a Two-row Velocity Stage

It is concluded that stage Nr 113 is of satisfactory efficiency under sub-critical conditions but beyond this it drops markedly and is still worse with expanding nozzles. However, the Moscow Power Institute stage KS-lA with a nozzle height of 25 mm and a diameter of 668 mm had the very high maximum internal efficiency of 81%, which confirmed the high efficiency of this combination at a low degree of reaction. Stage KS-lA was better than stage Nr 113 in efficiency and stability, particularly with partial steam supply. It should be borne in mind that stage Nr 113 is more carefully manufactured and has assembled milled nezzles, whereas stage KS-lA was tested with a welded diaphragm.
There are 13 figures, 1 table and 1 Soviet reference.

ASSOCIATION: MEI

1. Turbine wheels--Design 2. Turbine wheels--Test results

Card 5/5

3. Turbine wheels-Effectiveness

DEYCH, M.Ye., doktor tekhn.nauk; GUBAREV, A.V., inzh.

Studying turbine working cascades at high speed [with summary in English]. Teploenergetika 5 no.12:56-62 D 158. (MIRA 11:12)

1. Moskovskiy energeticheskiy institut.
(Turbines)



DETCH, M.Ye., doktor tekhn.nauk; ZARYANKIN, A.Ye., kand.tekhn.nauk

Approximate method for calculating the terminal losses [with summary in English]. Teploenergetika 5 no.9:57-60 S '58. (MIRA 11:10)

1.Moskovskiy energeticheskiy institut.
(Turbines)

DEYCH, M.Ye., prof. doktor tekhn. nauk; SAMOYLOVICH, G.S., dots. kand. tekhn.

Setup for automatizing the static tests of turbine cascades. Emergomashinostroenie 4 no.9:4-8 S '58. (MIRA 11:11)

(Turbines—Aerodynamics)

SOV/96-58-9-10/21

AUTHORS: Deych, M. Ye. (Doctor of Technical Science) and Zaryankin, A.Ya. (Candidate of Technical Science)

An Approximate Method of Calculating Terminal Losses in

Turbine Blading (Priblizhennyy metod rascheta kontsevykh

poter')

TITLE:

PERIODICAL: Teploenergetika, 1958, Nr 9, pp 57 - 60 (USSR)

ABSTRACT: A great deal of experimental data has been accumulated on the structure of flow in straight gratings of turbine blades and on the magnitude of terminal losses. The experimental results show that in a straight grating of turbine blades there is a complex spatial flow of working substance which cannot yet be calculated adequately. Existing methods of evaluating terminal losses depend on a number of simplifying assumptions. It is, therefore, of interest to attempt to derive a formula for these losses. Formula 16 is then derived: one of its factors is a function of the dimensionless velocity, and can be obtained from the curve given in

Card 1/2 Fig 1. Numerical values of the other two factors in the formula can be determined from Fig 2, which gives a graph

sov/96-58-9-10/21. An Approximate Method of Calculating Terminal Losses in Turbine Blading

of experimental data for terminal losses obtained for impulse and reaction blading with different values of pitch, height and inlet and outlet angles. It is concluded that the coefficients depend on the flow conditions in the boundary layer and on the type of blading. Allowing that the results given in Fig 2 were made in different laboratories with different experimental procedures, the scatter of the results is acceptable. Values of the coefficients of the results is acceptable. Values of the coefficients to be used in the formula that have been derived from the test results are tabulated.

There are 2 figures, 1 table, 4 literature references (Soviet)

ASSOCIATION: Moskovskiy energeticheskiy Institut (Moscow Power Institute)

1. Turbine blades--Performance 2. Mathematics--Applications

Card 2/2

500/96-58-12-10/18

AUTHORS:

Devah M. Te . (Dr . Te : h . Sei.)

Gubarev, A. . (Engineer)

TITLES

The investigation of working blades of turbines at high speed. (Issledovanta rebookikh reshetok tratia pra bolishikh shorestynkh

PERIODICAL 8

Taplocmergethia, 1958, No. 12. pp. 56-62 (VESE)

ABSTRACTS

As there are no theoretical methods of designing turbine blading for soper-cratical speeds, experimental developments ascens great importance. At supergonna speeds the leading edge most be as sharp as possible and the bank inlat face should only have slight compature. To smoure atable flow in the channel between the blades it is necessary to avoid severe somelenation on the back profile. One way of doing this is to profile the back of the blade in such a way that there is steady constriction of the flow up to the inlet section of the charmed between the blades. Because of the mature of the resultant flow, while needed may be sailed etap when reterdation of flow. A second method of sobjecting this object is to make the surrecture at the inlet section of the hear of the blade to spands quade and transcript that there is a share stateme as velocity before the blade, at low supersonic speeds the second method and be nessed, at high supersonic speeds the everywish retardation of flew is preferables alterratively, the channel patween the blades way be never that so that the jump secure within the channel and rethidenion takes place in a system of stape

Card 3/3

The investigation of working blades of turbines at high speed.

50V/98-58-12-10/18

of compression on a small inlet section of the channel. The interblade channel should be either expanding (first method) or contractingexpanding (second method). The main types of blade profile are illustrated in Fig.1; Fig.la. shows profile type A intended for subcritical speeds of Mach 0.9; Fig.lb. shows profile type B intended for Mach 0.9 - 1.25; Fig.lc. illustrates profile type C using the method of stepwise retardation, and Fig.ld. shows the profile type C using the direct jump method. Both class C profiles are used for high supersonic speeds of Mach greater than 1.3. An article by Deych and others in Teploenergetika, 1956, No. 5. gave a notation of blading and profiles which is adopted here. The pressure distribution over profile TR-1B, seen in Fig.3., ha nationably dissimilar and the differences are discussed. Cornesponding empres over profile TR-2B, which is designed to turn the fllow through smaller angles, are presented in Fig.4. Velocity distribution curves over profile TR-1B with somewhat different angles, are given in Fig. 5. The distributions of lagges over the height of the blading are platted in Fig. 6., and the merits of the different bladings are compared. Graphs of profils losses in group B blades appear in Fig. 7. Total loss tarves for different types of blading are given in Fig. 8. Flots of supersonic flow in turbins blading are sketched in Fig. 9: the dafference between

Card 2/3

The investigation of working blades of turbinss at high speed.

SOV/96-58-12-10/18

the flow in type A blades (Fig. 9a) and type B blades (Fig. 9b) is explained. The distribution of the flow outlet angle over the height of blading TR-IB is graphed in Fig. 10. The terminal livenes and the Mach number are related graphically in Fig. 11., demonstrating that losses diminish rapidly as the Mach number increases. At he concluded that for Mach numbers of 0.9 - 1.0 it is necessary to not blades of group A. Blades of these profiles have low loanes and stable characteristics over a wide range of angles of flow inlet. For Math numbers of 0.9 - 1.25 the profiles should have sharp inlat adges and small curvature of the back of the blade on the inlet section: also, there should preferably be straight sections in the region of the inlet and outlet edges. Profiles of group B cannot be used for high supersonic speed. The curves of total losses given in Rig. 8. include two related to bhades of group C designed in accordance with the principles explained in the article. Freliminary test results have shown the correctness of the basic idea and a new series of blading should accordingly be developed for high supersonic speeds. There are 11 figures and 7 references, 5 of which are Soviet.

ASSOCIATION: Moscow Power Institute (Moskorskiy Emergethobeakiy institut)

Card 3/3

10(0)

PHASE I BOOK EXPLOITATION

SOV/2214

Deych, Mikhail Yefimovich, and Georgiy Semenovich Samoylovich

- Osnovy aerodinamiki osevykh turbomashin (Fundamentals of the Aerodynamics of Axial-flow Turbomachinery) Moscow, Mashgiz, 1959, 427 p. Errata slip inserted. 3,500 copies printed.
- Reviewer: V.S. Beknev, Candidate of Technical Sciences; Eds.: A.N. Sherstyuk, Candidate of Technical Sciences, Docent, and A.Ye. Zaryankin, Candidate of Technical Sciences; Tech. Ed.: B.I. Model; Managing Ed. for Literature on General Technical and Transport Machine Building: V.I. Kubarev, Engineer.
- PURPOSE: This book is intended for engineers, scientific workers, and aspirants. It may also be used by students of advanced courses of power engineering institutes.
- COVERAGE: This book deals with theoretical and experimental work on the aerodynamics of axial-flow turbomachines and the methods of

Card 1/10

Fundamentals of the Aerodynamics (Cont.)

SOV/2214

analyzing the flow of viscous fluids and perfect fluids over aerodynamic cascades of blades. The results of systematic investigation of subsonic and supersonic flow in plane, straight, and annular cascades are given. It includes the basic aspects of threedimensional flow in the stages of turbomachines, and nonstationary and burble phenomena in the stages of axial-flow compressors. Methods for experimental investigation and the experimental apparatus are described. The book also gives ageneralization of some theoretical and experimental results obtained at the MEI (Moscow Power Engineering Institute) and other Soviet and non-Soviet organizations and laboratories. Much experimental material was obtained in the steam-and gas-turbine laboratory of the Moscow Power Engineering Institute (1957 included) by the gas-turbine group. The following persons took part in the investigations: Candidates of Technical Sciences B.M. Troyanovskiy, A.N. Sherst-yuk, V.A. Baranov; Engineers V.I. Abramov, L.Ye. Kiselev, Ye.V. Mayorskiy, I. Neruda, M.F. Zatsepin, V.P. Mayorskiy, G.A. Filippov, V.G. Filippova, Ye. V. Stekol'shchikov, V.P. Novoderezhkin, and Senior Laboratory Technicians N.S. Sokolov and P. D. Kustov. Many of the investigations were carried out in conjunction with the Kaluzhskiy turbinnyy zavod (Kaluga Turbine Plant) and the Lenin-

Card-2/10

Fundamentals of the Aerodynamics (Cont.)

SOV/2214

gradskiy metallicheskiy zavod (Leningrad Metalworking Plant). The experimental shop of the Kaluga Turbine Plant manufactured models for the experimental units of the steam-and gas-turbine department of the Moscow Power Engineering Enstitute. Some of the published materials on the investigation of valves and nozzles were submitted by the authors to the Leningrad Metalworking Plant and to the Kirovskiy zavod (Kirov Flant). Chapters III, VI, and VII, were written jointly by the authors; Chapters I, II, VIII, and XI were written by Samoylovich; Chapters IV, V, IX, and X, by M.Ye. Deych; Paragraphs 39, 40, 41, and 42 of Chapter VII were compiled by F.V. Kazintsev; Paragraphs 12 and 13 of Chapter III were written jointly with A. Ye. Zaryakin; Chapter V, was written jointly with A.V. Gubarev. In the text, the following Russian scientists are mentioned in connection with the development of turbomachinery in the USSR: N.Ye Zhukovskiy, S.A. Chaplygin, L.I. Sedov, N.Ye. Kochin, L.A. Simonov, E.L.Blokh, D.A. Voytashevskiy, G.Yu. Stepanov, M.I. Zhukovskiy, L.A. Dorfman, A.F. Lesokhin, A.I. Borisenko, B.L. Ginsburg, O.I. Novikova, F.I. Frankl, G.A. Buga-

Card 3/10

Fundamentals of the Aerodynamics (Cont.) SOV/2214 yenko, R.M. Fedorov, Yu.I. Shvets, L.G. Loytsyanskiy, L.Ye. Kalikhman, N.M. Markov, B.M.Yakob, G.Flyngel, N.A. Sknar', A.N. Krylov, I.I. Kirillov, G.N. Abramovich, M.A. Lement'yev, B.N. Yuryev, V.P. Vetchinkin, K.A. Umakov, V.V. Uvarov, V.G. Tyryshkin, S.I. Shevyakov, P.K. Kazandzhan, L.P. Lokoy, V.N. Yershov, A.M. Zavadovskiy, S.V. Grishchukov, S.M. Shlyakhtenko, and N.I. Panteleyev. TABLE OF CONTENTS: 3 Preface 5 6 Ch. I. Potential Flow Over an Aerodynamic Cascade of Blades Stating the problem and the selection of basic formulas 10 2. Flow over annular cascades 3. Flow over cascade of blades of arbitrary form 16 4. Examples of the calculation of turbine and compressor cas-24 cades of blades Calculation of aerodynamic cascades by the method of con-5. 34 secutive approximations Hodograph method. Derivation of basic formulas 39 Application of the method of a hodograph to the solution

APPROVED FOR RELEASE: 06/12/2000 CIA-RDP86-00513R000410310014-7"

05/16 been

DEYCH, M. Ye.; ROBOZHEV, A.V.

Ultimate conditions for jet compressors. Nauch.dokl.vys.shkoly; energ. no.1:175-180 '59. (MIRA 12:5)

1. Rekomendovana kafedroy parovykh i gazovykh turbin Moskovskogo energeticheskogo instituta. (Compressors--Aerodynamics)

SOV/96-59-4-7/21

Deych, M.Yc., Doctor of Technical Sciences; AUTHORS:

Troyanovskiy, B.M., Candidate of Technical Sciences;

Kazintsev, F.V, Engineer and Abramov, V.I., Engineer

TITLE:

An Investigation of a Series of Single-row Stages

(Issledovaniye serii odnovenechnykh stupeney)

PERICDICAL: Teploenergetika, 1959, Nr 4, pp 38-43 (USSR)

ABSTRACT:

A number of types of nozzle and working blading for turbines have been developed in the Moscow Power Institute. These can be combined in various ways in single- and tworow stages. Tests results on a number of two-row velocity stages have already been published in Teploenergetika, 1958, Nr 5. Six combinations of single-row stages were made up of blading intended for operation at subsonic and sonic velocities. The stage combinations consisted of two nuzzle and three working blades. All the stages were 534 mm diameter, 25 mm nozzle blade height and 28 mm working blade height and were all of the same width. stage diagram is given in Fig.1. The experimental steam turbine and the procedure used were the same as described in Teploenergetika, 1957, Nr 5. Particulars of the stages

Card 1/4

80V/96-59-4-7/21

An Investigation of a Series of Single-row Stages

tests are tabulated. The stages were first tested with full steam supply. Experimental internal efficiency data for stage KD-2-2A are given in Fig.2. Where high supersonic speeds are used the blading losses increase and the stage efficiency is reduced. Fig.3 gives losses in nozzle blading TS-2A and the internal efficiency of stage KD-2-2A. Mean reaction curves for stage KD-2-2A are given in Fig.4. Internal efficiency curves for all six combinations investigated are given in Fig.5 and the results are discussed. Stage KD-2-2A was then tested with partial steam supply. Curves of the relative internal efficiency of the stage are given in Fig.6. Internal efficiency curves for the stage with different angles of steam delivery are given in Fig.7. It will be seen that the stage efficiency is much reduced with partial steam supply. This and other test results are discussed and are stated to be fully in accordance with theoretical expectations. The influence of nozzle diaphragm widths on stage efficiency of KD-2-1A was then investigated and

Card 2/4

SOV/96-59-4-7/21

An Investigation of a Series of Single-row Stages

the results are given in Fig.8. It is clearly shown that the stage efficiency falls off with a wide diaphragm and this is because the tests were made outside the zone of best width. The efficiencies of single- and two-row stages are then compared. The test results for two such stages are given in Fig. 10 and show the conditions under which one or other of the two regulating stages should be selected. The number of unregulated stages and other constructional features of a machine vary considerably depending on the type of regulating stage used. A detailed analysis of this problem falls outside the scope of the present article. It is concluded that the single-row stages investigated are of high efficiency, particularly the stages KD-2-2A and KD-1-2A. If the gaps are right and the blading is correctly chosen a small negative reaction has little influence on the efficiency of a single row stage with short blades. On the basis of the tests it is considered that for the high and medium pressure cylinders of turbines the best two combinations are KD-2-2A and KD-1-2A composed of blade profiles TS-2A, TR-2A, TS-1A and TR-2A. Investigations on stage KD-2-2A with partial

Card 3/4

SOV/96-59-4-7/21

An Investigation of a Series of Single-row Stages

steam supply and various numbers of nozzles showed that the important effect of additional lesses and secondary effects associated with partial steam supplies. Comparison of single- and two-row stages made of the new improved blade prefiles shows that the difference between the possible highest efficiency of these stages has been reduced and the field of application of a velocity stage has been extended. There are 10 figures, I table and 2 Soviet references.

ASSOCIATION: Moskovskiy Energeticheskiy Institut (Moscow Power Institute)

Card 4/4

DEYCH, M.Ye., doktor tekhn.nauk, prof.; KAZINTSEV, F.V., inzh.; GOLOVIN, V.A., inzh.

Automatic computing device for solution of energy-loss equations used in the study of turbine bladings. Energonashinostroenie 5 no.3:31-34 Mr. 159. (MIRA 12:3)

(Turbines)

AUTHORS: Deych, M.Ye., (Dr. Tech.Sci.), Kazintsev, F.V., Abramov, V.I., Kiselev, L.Ye. and Filippova, V.G.

(Engineers)

TITLE: An Investigation of Turbine Stages with Long Blades of Constant Profile under Variable Conditions (Issledovaniye peremennogo rezhima turbinnykh stupenei s dlinnymi lopatkami postoyannogo profilya)

PERIODICAL: Teploenergetika, 1959, Nr 6, pp 8-17 (USSR)

ABSTRACT: This article describes the results of tests on four single-row stages with relatively long blades of constant profile, fitted to an experimental turbine. The efficiency of single-row stages depends on a number of geometrical and operating conditions: the configuration, pitch and angles of installation of the blades, the ratio of the flow areas, the velocity ratio and the Mach and Reynolds numbers. The tests described here were made to study the influence of these factors on the efficiency. The stages had a d/2 ratio + 7.73 which is the limiting value for cylindrical blading. The four stages investigated employed two types of guide vanes (TS-1A and TS-2A) and two types of working blades (TR-2A and TR-3A).

SOV/96-59-6-2/22

An Investigation of Turbine Stages with Long Blades of Constant Profile under Variable Conditions

The principal geometrical characteristics of the blading are given in Table ... All the stages used welded diaphragms of 400 mm mean diameter with guide vanes 48 mm high and working blades 51.7 mm high. The measuring equipment used is briefly described. The stages were tested with ratios of back pressure to inlet pressure of 0.9 to 0.54, which corresponds to a Mach number range of 0.4 to 1.0. The tests were made with constant back pressure. The influence of diaphragm leakage on the efficiency and the degree of reaction at root and tip sections were investigated. The quantity of leakage steam ranged from 0.8 to 3.5% of the flow through the guide vanes. The influence of the Reynolds number on the stage characteristics was investigated in three of the stages, with Reynolds numbers ranging from 3 x 105 to 7 x 10 5 The maximum error in determining the stage efficiency was between 0.4 and 0.6%. The influence of compressibility on the stage efficiency and degree of Card 2/8 reaction is then considered. Stage efficiency graphs as functions of velocity and pressure ratios are given in

SOV/96-59-6-2/22

An Investigation of Turbine Stages with Long Blades of Constant Profile under Variable Conditions

Fig 1: it will be seen that for each stage there is a pressure ratio that gives maximum efficiency. Values of the best pressure ratio, the highest efficiency, and the change in efficiency as the pressure ratio deviates from the optimum value, are tabulated in Table 2. The curves in Fig 1 show that the efficiency is fairly stable as the velocity ratio changes, indicating that stages with guide vanes type TS-2A have a flatter characteristic as a function of the velocity ratio. This is because the ratio of the blade area to the guide-vane area is lower and there is consequently more reaction in stages with these guide vanes. Curves of stage efficiency as a function of M_0 with constant velocity ratio are given in Fig 2a, and curves of efficiency as function of the available heat drop with the speed constant in Fig 2b. From consideration of these curves it is concluded that the stage efficiency is reasonably stable. Curves of the pressure distribution over the pitch of the guide Card 3/8 vanes at the tip and root sections respectively are given

in Figs 3a and 3b. Corresponding curves under static